

# MMIC Design and Technology

## Amplifier Design

Instructor Dr. Ali Medi

# Data file for actual device

! FILENAME: N67300.S2P VERSION: 1.0  
! NEC PART NUMBER: NE67300 DATE: 4/83  
! BIAS CONDITIONS: VDS=3V, IDS=10mA  
! NOTE : GATE AND DRAIN BOND WIRES ARE DE-EMBEDDED.  
! NOTE : SOURCE BOND WIRE EFFECTS ARE INCLUDED. Ltotal = 0.07 nH  
! (4 EACH 0.7 mil DIAMETER GOLD WIRES APPROXIMATELY 0.015" LONG).

# GHZ S MA R 50

2	0.95	-26	3.79	161	0.04	79	0.59	-13
4	0.89	-50	3.26	141	0.06	66	0.58	-24
6	0.82	-70	2.83	126	0.08	56	0.54	-33
8	0.78	-88	2.55	114	0.09	51	0.5	-42
10	0.73	-102	2.21	104	0.1	48	0.47	-48
12	0.71	-114	2.16	93	0.1	43	0.45	-55
14	0.71	-122	2.11	90	0.11	44	0.47	-62
16	0.67	-128	1.92	76	0.11	43	0.49	-64
18	0.66	-140	1.81	63	0.11	40	0.52	-70

# Stability

- Transistor is unstable when  $|\Gamma_{in}| > 1$

$$\Gamma_{in} = \frac{b_1}{a_1} = S_{11} + \frac{S_{21}S_{12}\Gamma_L}{1 - S_{22}\Gamma_L}$$

## Boundary Condition for Stability

$$\left| S_{11} + \frac{S_{21}S_{12}\Gamma_L}{1 - S_{22}\Gamma_L} \right| = 1$$

# Stability

- Transistor is unstable when  $|\Gamma_{out}| > 1$

$$\Gamma_{out} = \frac{b_2}{a_2} = S_{22} + \frac{S_{21}S_{12}\Gamma_s}{1 - S_{11}\Gamma_s}$$

## Boundary Condition for Stability

$$\left| S_{22} + \frac{S_{21}S_{12}\Gamma_s}{1 - S_{22}\Gamma_s} \right| = 1$$

# Stability Circles on Smith Chart

- Load or Source stability circle is the locus of points in the  $\Gamma_L$  or  $\Gamma_s$  plane, for which  $\Gamma_{in}$  or  $\Gamma_{out} = 1$ . If the center of the smith chart is enclosed by the stability circle then all points inside the circle are stable. If the center is not enclosed then all points inside the circle are unstable.

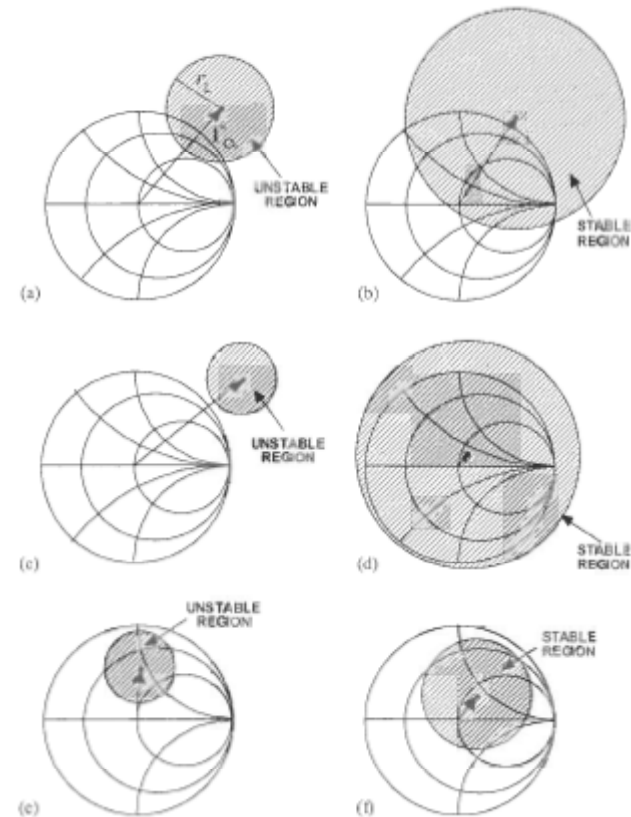


Figure 5.2 Stability circles on the Smith chart: (a) stability circle partially inside the Smith chart, (b) partially inside and encompassing the 50  $\Omega$  point, (c) completely outside, (d) completely encompassing the Smith chart, (e) completely inside but not encompassing the 50  $\Omega$  point and (f) completely inside and encompassing the 50  $\Omega$  point

# Unconditional Stability

- If all of the smith chart is in a stable region then the transistor is said to be unconditionally stable.
  - $\Gamma_{in}$  or  $\Gamma_{out} < 1$  for all values of  $\Gamma_L$  or  $\Gamma_S$

$$K = \frac{1 - |S_{11}|^2 - |S_{22}|^2 + |\Delta|^2}{2|S_{12}S_{21}|}$$

**Unconditionally Stable for  $K > 1$**

$$\Delta = S_{11}S_{22} - S_{12}S_{21}$$

# Constant Gain Circles

$G_T$  = Power delivered to load / Power available from source

$$G_T = \frac{|S_{21}|^2 (1 - |\Gamma_s|^2) (1 - |\Gamma_L|^2)}{|1 - S_{11}\Gamma_s - S_{22}\Gamma_L + \Delta\Gamma_s\Gamma_L|^2}$$

$$G_{TU}$$

When  $S_{12}=0$ ,  $G_{TU}=G_s G_o G_L$

$$G_s = \frac{1 - |\Gamma_s|^2}{|1 - S_{11}\Gamma_s|^2}$$

$$G_o = |S_{21}|^2$$

$$G_L = \frac{1 - |\Gamma_L|^2}{|1 - S_{22}\Gamma_L|^2}$$



# MAG

$$MSG = \left| \frac{S_{21}}{S_{12}} \right|$$

$$K < 1$$

$$MAG = \left| \frac{S_{21}}{S_{12}} \right| \left( K - \sqrt{K^2 - 1} \right)$$

$$K > 1$$

# Noise Figure

$$F = F_{\min} + 4R_n \frac{|\Gamma_s - \Gamma_{opt}|^2}{(1 - |\Gamma_s|^2) |1 + \Gamma_{opt}|^2}$$

$F_{\min}$  is noise figure at  $\Gamma_{opt}$

$R_n$  is normalized “noise resistance”

Circles of constant noise figure in  $\Gamma_s$  Plane

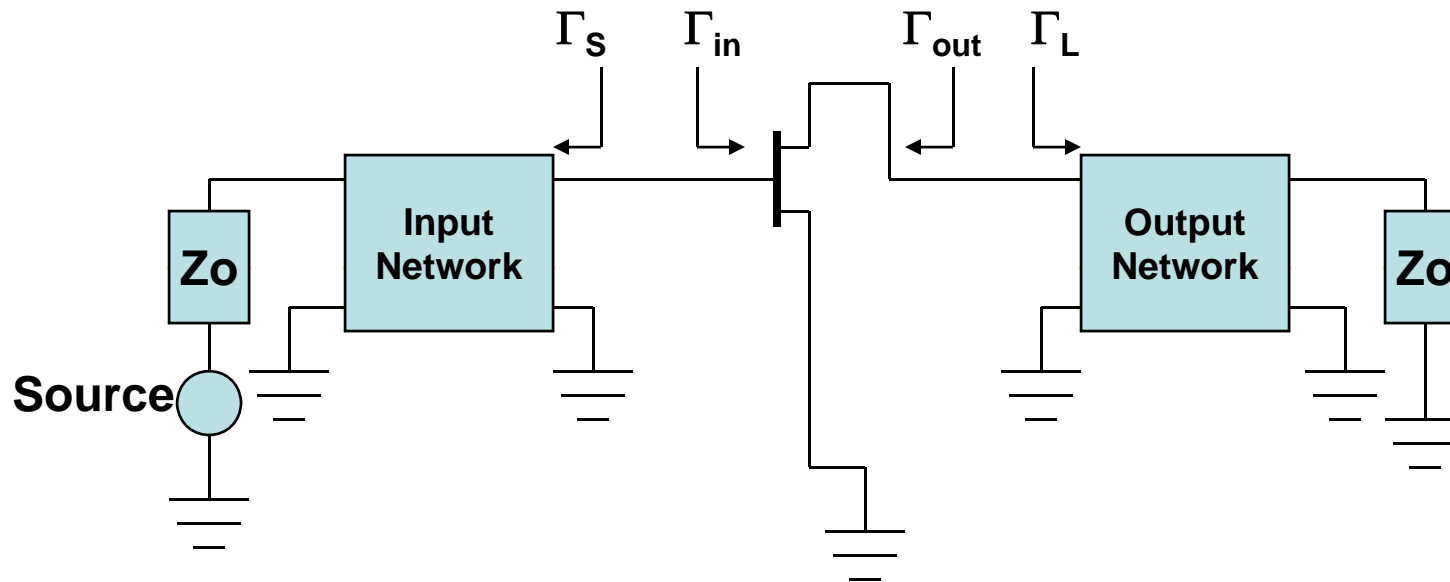
# Device Data File

! NEC PART NUMBER: NE67300      DATE: 4/83  
! BIAS CONDITIONS: VDS=3V, IDS=10mA  
! NOISE PARAMETERS  
! NOTE : GATE AND DRAIN BOND WIRES ARE DE-EMBEDDED.  
! NOTE : SOURCE BOND WIRE EFFECTS ARE INCLUDED. Ltotal = 0.07 nH  
!     (4 EACH 0.7 mil DIAMETER GOLD WIRES APPROXIMATELY 0.015" LONG).

1	0.40	.90	12	.57
2	0.40	.85	21	.51
4	0.40	.75	40	.44
6	0.60	.69	55	.38
8	0.80	.62	70	.33
10	1.10	.56	85	.28
12	1.40	.52	99	.24
14	1.70	.49	114	.20
16	2.00	.47	127	.18
18	2.25	.45	140	.16

FORMAT				
GHz	NF <sub>min</sub> dB	$\Gamma_{opt}$ Mag	$\Gamma_{opt}$ angle	normalized Rn

# Design Process



Design  $\Gamma_s$  and  $\Gamma_L$  to provide the desired performance  
May be a trade with stability, gain, noise figure  
Then design matching networks

# Design Process

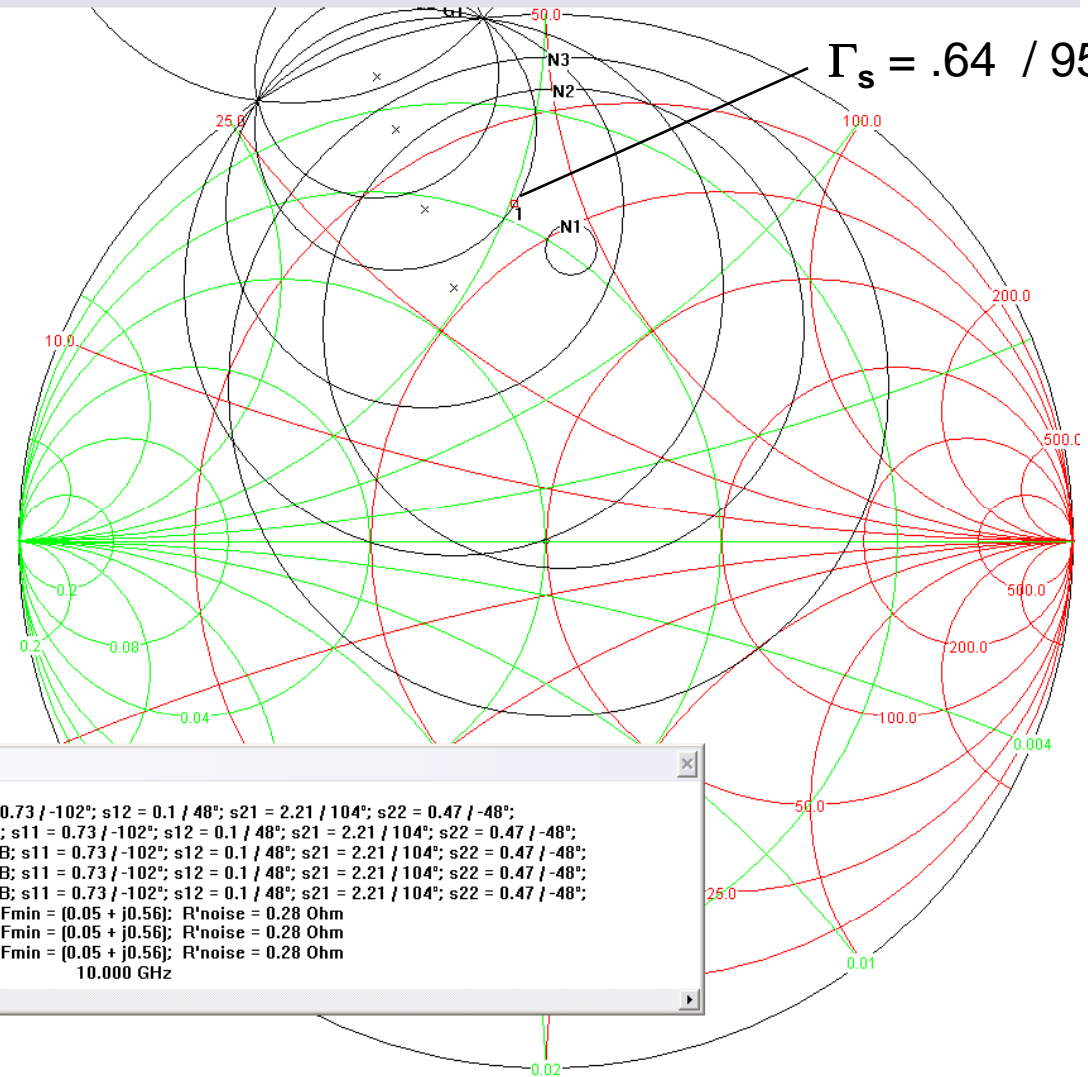
- Plot on  $\Gamma_s$  plane
  - Source stability circle
  - Constant Gain circles
  - Constant Noise Figure circles
- Choose a suitable value of  $\Gamma_s$

$\Gamma_s = .64 / 95.3 \text{ deg}$

Schematic

Toolbox

SERIES  
C L R  
LINE  
SHUNT  
C L R  
LINE  
TRANSF.  
DATAPoint



Data Points

S1: input plane stability circle; stable outside;  $K = 0.75$ ;  $s_{11} = 0.73 / -102^\circ$ ;  $s_{12} = 0.1 / 48^\circ$ ;  $s_{21} = 2.21 / 104^\circ$ ;  $s_{22} = 0.47 / -48^\circ$ ;  
 G1: input plane const. gain circle;  $G_{max} = 13.4\text{dB}$ ;  $V_p = 8.0 \text{ dB}$ ;  $s_{11} = 0.73 / -102^\circ$ ;  $s_{12} = 0.1 / 48^\circ$ ;  $s_{21} = 2.21 / 104^\circ$ ;  $s_{22} = 0.47 / -48^\circ$ ;  
 G2: input plane const. gain circle;  $G_{max} = 13.4\text{dB}$ ;  $V_p = 10.0 \text{ dB}$ ;  $s_{11} = 0.73 / -102^\circ$ ;  $s_{12} = 0.1 / 48^\circ$ ;  $s_{21} = 2.21 / 104^\circ$ ;  $s_{22} = 0.47 / -48^\circ$ ;  
 G3: input plane const. gain circle;  $G_{max} = 13.4\text{dB}$ ;  $V_p = 12.0 \text{ dB}$ ;  $s_{11} = 0.73 / -102^\circ$ ;  $s_{12} = 0.1 / 48^\circ$ ;  $s_{21} = 2.21 / 104^\circ$ ;  $s_{22} = 0.47 / -48^\circ$ ;  
 G4: input plane const. gain circle;  $G_{max} = 13.4\text{dB}$ ;  $V_p = 13.4 \text{ dB}$ ;  $s_{11} = 0.73 / -102^\circ$ ;  $s_{12} = 0.1 / 48^\circ$ ;  $s_{21} = 2.21 / 104^\circ$ ;  $s_{22} = 0.47 / -48^\circ$ ;  
 N1: constant 1.11dB noise figure circle;  $NF_{min} = 1.10\text{dB}$ ;  $r_{NFmin} = (0.05 + j0.56)$ ;  $R'_{noise} = 0.28 \text{ Ohm}$   
 N2: constant 2.00dB noise figure circle;  $NF_{min} = 1.10\text{dB}$ ;  $r_{NFmin} = (0.05 + j0.56)$ ;  $R'_{noise} = 0.28 \text{ Ohm}$   
 N3: constant 3.00dB noise figure circle;  $NF_{min} = 1.10\text{dB}$ ;  $r_{NFmin} = (0.05 + j0.56)$ ;  $R'_{noise} = 0.28 \text{ Ohm}$   
 DP-Nr. 1             $[19.1 + j41.8]\text{Ohm}$              $Q = 2.2$              $10.000 \text{ GHz}$

Zo  
50.0 Ohm

VSWR	Q	r	Y	Z
39.2 : 1	3.45	0.95 / -169.85°	0.0602 + j0.2079	1.28 - j4.44

Lecture 6 Amplifier Design

# Design Process

- Calculate  $\Gamma_{out}$

$$\Gamma_{out} = S_{22} + \frac{S_{21}S_{12}\Gamma_s}{1 - S_{11}\Gamma_s}$$

For example data

When  $\Gamma_s = .64 / 95.3 \text{ deg}$

$\Gamma_{out} = 0.61 / -71.9 \text{ deg}$

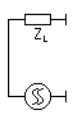
# Design Process

- Plot on  $\Gamma_L$  plane
  - Load stability circle
  - Conjugate of  $\Gamma_{out} = \Gamma_{out}^*$
- If  $\Gamma_{out}^*$  is an allowed value for  $\Gamma_L$ 
  - Choose  $\Gamma_L = \Gamma_{out}^*$
- Else
  - Plot Constant Gain circle on  $\Gamma_L$  plane
  - Select a suitable value of  $\Gamma_L$



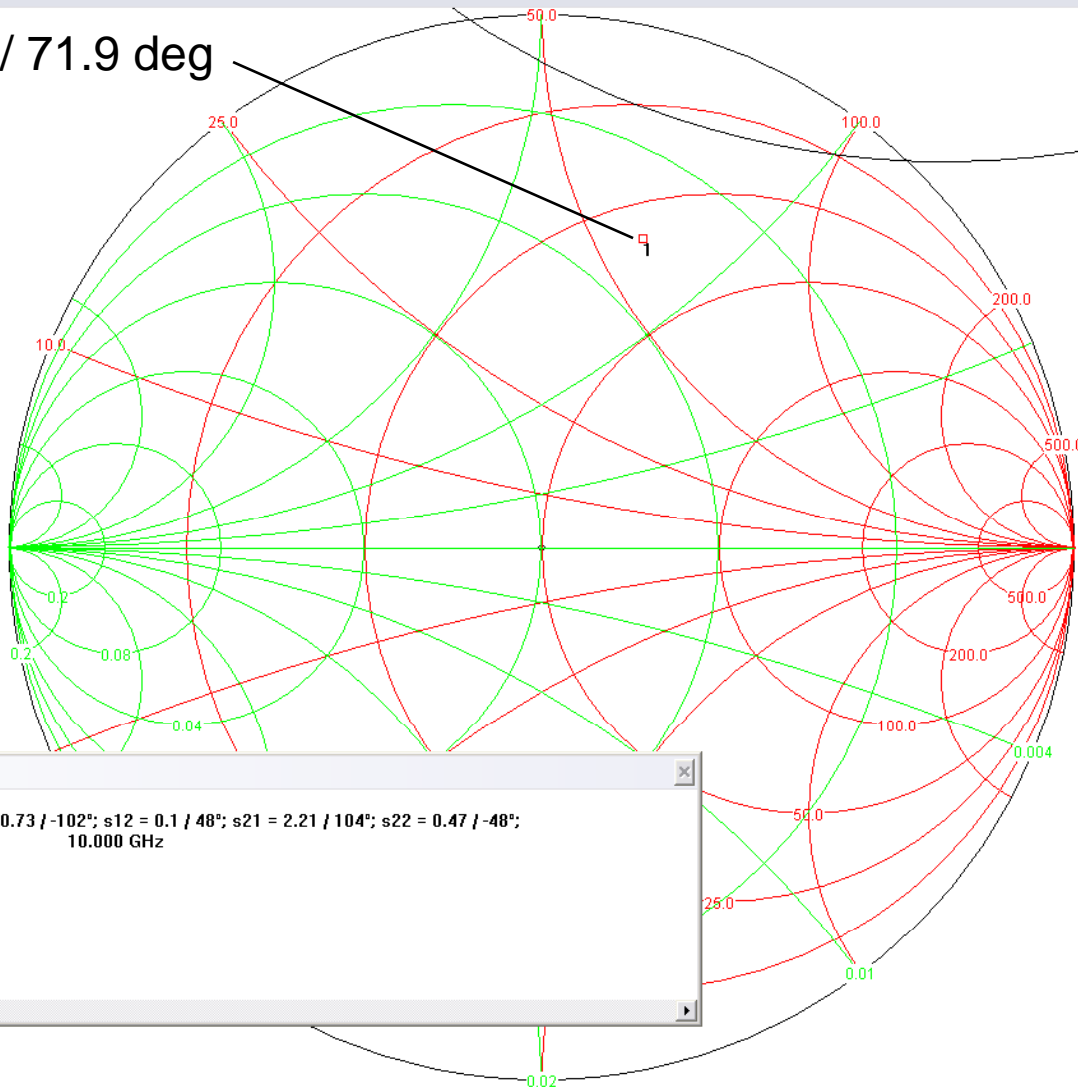
$$\Gamma_L = .61 / 71.9 \text{ deg}$$

Schematic



Toolbox

- SERIES
  - C
  - L
  - R
- LINE
- SHUNT
  - C
  - L
  - R
- LINE
- TRANSF.
- DATAPoint



Data Points

S1: output plane stability circle; stable outside; K = 0.75; s11 = 0.73 / -102°; s12 = 0.1 / 48°; s21 = 2.21 / 104°; s22 = 0.47 / -48°;  
 DP-Nr. 1            (31.6 + j58.4)Ohm            Q = 1.8            10.000 GHz

Zo  
50.0 Ohm

VSWR	Q	r	Y	Z
2.1 : 1	0.83	0.36 / -82.83°	0.0142 + j0.0118	41.64 - j34.68

### Lecture 6 Amplifier Design

# Calculate Gain

$$G_T = \frac{|S_{21}|^2 (1 - |\Gamma_s|^2) (1 - |\Gamma_L|^2)}{|1 - S_{11}\Gamma_s - S_{22}\Gamma_L + \Delta\Gamma_s\Gamma_L|^2}$$

$$\Delta = S_{11}S_{22} - S_{12}S_{21}$$

For our example  $G_T = 15.8$   
 $10\text{Log } G_T = 12.0 \text{ dB}$

# Calculate Noise Figure

$$F = F_{\min} + 4R_n \frac{|\Gamma_s - \Gamma_{opt}|^2}{(1 - |\Gamma_s|^2) |1 + \Gamma_{opt}|^2}$$

## Some useful Excel functions (must install Analysis ToolPak)

<b>IMABS</b>	Returns the absolute value (modulus) of a complex number
<b>IMAGINARY</b>	Returns the imaginary coefficient of a complex number
<b>IMARGUMENT</b>	Returns the argument theta, an angle expressed in radians
<b>IMCONJUGATE</b>	Returns the complex conjugate of a complex number
<b>IMCOS</b>	Returns the cosine of a complex number
<b>IMDIV</b>	Returns the quotient of two complex numbers
<b>IMEXP</b>	Returns the exponential of a complex number
<b>IMLN</b>	Returns the natural logarithm of a complex number
<b>IMLOG10</b>	Returns the base-10 logarithm of a complex number
<b>IMLOG2</b>	Returns the base-2 logarithm of a complex number
<b>IMPOWER</b>	Returns a complex number raised to an integer power
<b>IMPRODUCT</b>	Returns the product of from 2 to 29 complex numbers
<b>IMREAL</b>	Returns the real coefficient of a complex number
<b>IMSIN</b>	Returns the sine of a complex number
<b>IMSQRT</b>	Returns the square root of a complex number
<b>IMSUB</b>	Returns the difference between two complex numbers
<b>IMSUM</b>	Returns the sum of complex numbers

# Design Input and Output Network

- Input network transforms the source impedance such that  $\Gamma_s$  is presented to the transistor
- Output network transforms the load impedance such that  $\Gamma_L$  is presented to the transistor

# Biasing

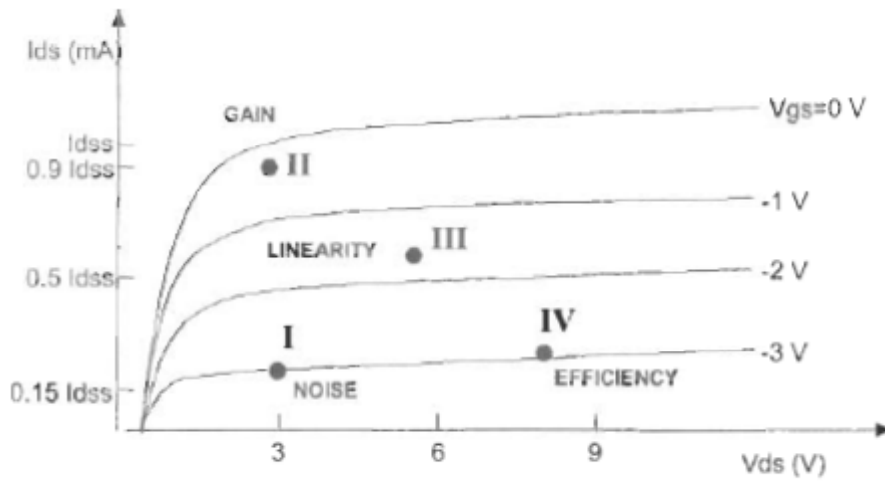


Figure 5.12 Typical FET I-V curves and operating bias points

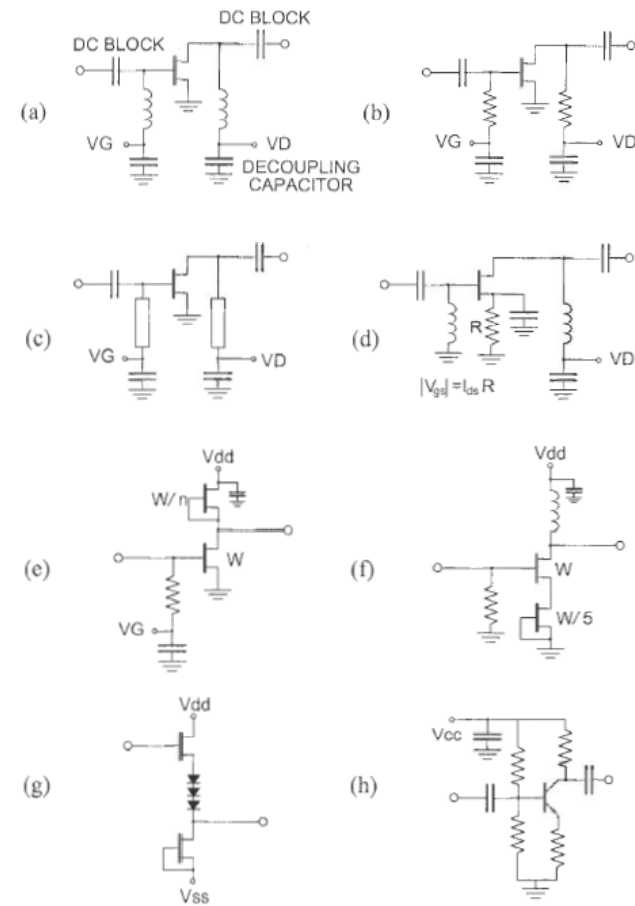


Figure 5.13 DC bias networks: (a) inductors as bias chokes, (b) high value resistors, (c) microstrip stubs, (d) self-biasing, (e) active load, (f) constant-current source self-biasing, (g) DC coupling and (h) bipolar transistor biasing