



**Sharif University of Technology
School of Mechanical Engineering
Center of Excellence in Energy Conversion**

Advanced Thermodynamics

Lecture 13

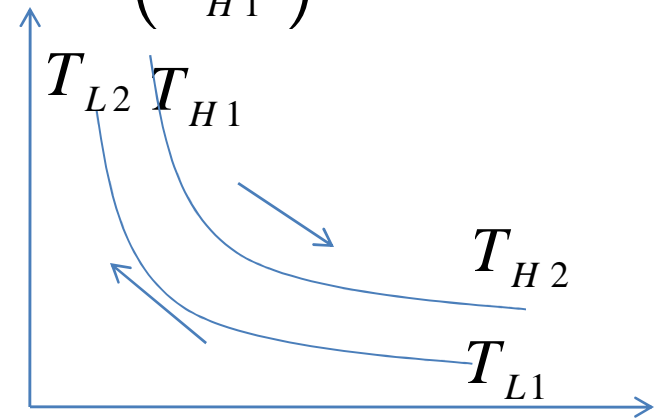
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2011

Ø For simplification, consider an average temperature for hot and cold flows, namely eutropic average temperature.

$$T_{SA, H} \equiv \frac{\dot{Q}_H}{\int \frac{d\dot{Q}_H}{T_H}} = \frac{-m_H c_H (T_{H2} - T_{H1})}{-m_H c_H \int \frac{dT_H}{T_H}} \Rightarrow T_{SA, H} = \frac{(T_{H2} - T_{H1})}{\ln\left(\frac{T_{H2}}{T_{H1}}\right)}$$

$$T_{SA, L} = \frac{(T_{L2} - T_{L1})}{\ln\left(\frac{T_{L2}}{T_{L1}}\right)}$$



Ø 2nd Law of thermodynamics:

$$h = \frac{\dot{Q}_H - \dot{Q}_L}{\dot{Q}_H} = 1 - \frac{T_{SA, L}}{T_{SA, H}} - \frac{T_{SA, L} \dot{S}_{gen}}{\dot{Q}_H}$$

$$\dot{S}_{gen} = \frac{-\dot{Q}_H}{T_{SA, H}} + \frac{\dot{Q}_L}{T_{SA, L}} \rightarrow \dot{S}_{gen} = \dot{Q}_L \left[\frac{1}{T_{SA, L}} - \frac{1}{T_{SA, H}} \right]$$

∅ Investigation of exergy Eq. terms at different situations:

∅ If a system is in contact with only one source:

$$\left. \begin{array}{l} \Delta u = q - w \\ \Delta s = \frac{q}{T} + s_{gen} \end{array} \right\} \Rightarrow \Delta u - T_0 \Delta s = q \left(1 - \frac{T_0}{T}\right) - w - T_0 s_{gen}$$

$$\Rightarrow \Delta u + P_0 \Delta v - T_0 \Delta s = q \left(1 - \frac{T_0}{T}\right) - (w - P_0 \Delta v) - T_0 s_{gen}$$

$$\Delta(u + P_0 v - T_0 s) = \Delta\Phi \quad \text{Exergy or Availability}$$

$$\Delta u + P_0 \Delta v - T_0 \Delta s = (u_2 - u_1) + P_0 (v_2 - v_1) - T_0 (s_2 - s_1) = \Phi_2 - \Phi_1$$

$$\Rightarrow W_{rev, 1-2} = \Phi_1 - \Phi_2 = -\Delta\Phi$$

$$\frac{dy}{dt} = \sum_{i=1}^n \left(1 - \frac{T_0}{T}\right) \dot{Q}_i - \left(\dot{W}_{C.V.} - P_0 \frac{dV}{dt} \right) + \sum_{in} \dot{m} - \sum_{out} \dot{m} - T_0 \dot{S}_{gen}$$

∅ $\sum_{in} \dot{m} - \sum_{out} \dot{m}$: Net availability convected into the C.V. with mass flow, also called physical exergy, can be split into thermal and pressure components.

∅ For an ideal gas with constant heat capacity, c_p

$$E_{Ph.} = c_p \left[(T - T_0) - T_0 \ln \left(\frac{T}{T_0} \right) \right] + RT_0 \ln \left(\frac{P}{P_0} \right)$$

∅ For solids and liquids ($c_p = c_v = c$)

$$E_{Ph.} = -c (T - T_0) \ln \left(\frac{T}{T_0} \right) + v_m (P - P_0)$$

∅ v_m is the specific volume determined at T_0

- ∅ The chemical exergy, Ex_{chem} at P_0 can be calculated by bringing the pure component in chemical equilibrium with the environment.

$$Ex_{chem} = RT_0 \ln \left(\frac{P_0}{P_{ref}} \right)$$

- ∅ When a substance does not exist in the environment, it must first react to reference substances in order to get in equilibrium with the environment.

- ∅ The reaction exergy of reference condition needs Gibbs free energy changes.

$$\Delta G^0 = \Delta H^0 - T_0 \Delta S^0$$

$$Ex_{chem} = \sum_{i=1}^n \nu_i Ex_{chem,ref} - \Delta G^0$$

∅ Exergy analysis (2nd law analysis), 2nd law efficiency

$$\text{Heat Engines: } h_{2^{\text{nd}} \text{ law}} = \frac{W_{\text{actual}}}{W_{\text{reversible}}}$$

$$\text{Non-Cyclic Process: } h_{2^{\text{nd}} \text{ law}} = \frac{W_{\text{actual}}}{-\Delta\Phi} = \frac{W_{\text{actual}}}{W_{\text{rev}}}_{1-2}$$

∅ Energy analysis (1st law analysis), 1st law efficiency

$$\text{Heat Engines: } h_{th} = \frac{W}{Q_H}$$

$$\text{Non-Cyclic Process: } h_{is} = \frac{W_{\text{actual}}}{W_{\text{isentropic}}}$$